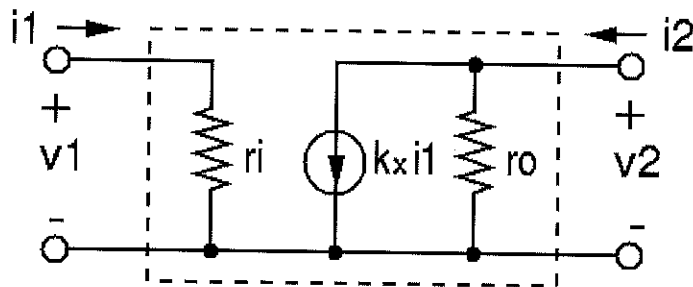


Name

1) BJT Model Parameters

The linear equivalent circuit of a BJT looks as follows



BJT Parameters:

$$V_T = 30 \text{ mV}$$

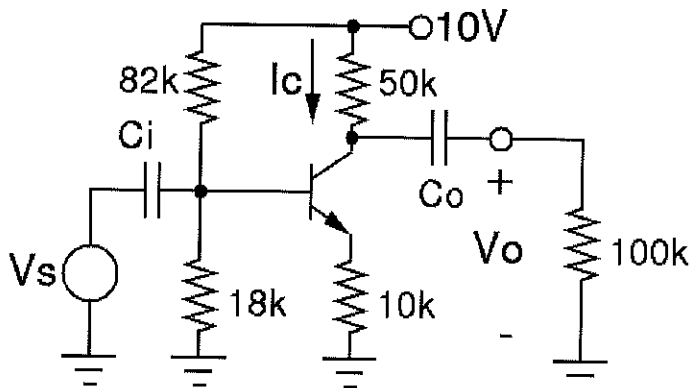
$$V_A = 60 \text{ V}$$

$$\beta = 100$$

$$I_{CQ} = 0.6 \text{ mA}$$

- Find values for r_i and r_o if the BJT is used in a **common emitter** configuration.
- Find values for r_i and r_o if the BJT is used in a **common base** configuration.
- Derive a value for the **voltage ratio** $A_v = v_2/v_1$ for the circuit shown if the BJT is used in a **common base** configuration.

2) Common Emitter Amplifier



BJT Parameters:

$$V_T = 30 \text{ mV}$$

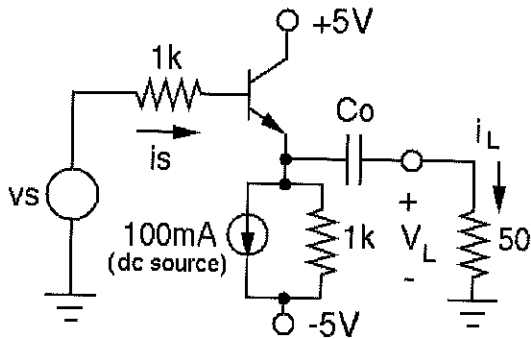
$$V_A = 60 \text{ V}$$

$$\beta = 100$$

$$V_{BEQ} = 0.7 \text{ V}$$

- Find values for I_{CQ} and V_{CEQ} .
- Determine C_i such that it forms a **low-frequency** corner at **100 Hz**.
- Derive an **expression** and a **value** for the voltage gain $A_v = v_o/v_s$ (assume that C_i and C_o act as **shorts** for the frequencies of interest).

3) Common Collector Amplifier



BJT Parameters:	
$V_T = 30 \text{ mV}$	
$V_A = \infty$	
$V_{BEQ} = 0.7 \text{ V}$	
$\beta = 100$	

- Find values for I_{CQ} and V_{CEQ} (Note: v_s is an ideal ac voltage source).
- Determine values for the input resistance R_{in} (seen at the base of the transistor) and the output resistance R_{out} (seen at the emitter). Assume that C_o acts as a short when calculating of R_{in} .
- What is the current gain $A_I = i_L / i_s$ of this transistor gain stage?

4) Quick Answer Questions

- Assume that R_E of the BJT amplifier in problem 2) is bypassed with a large capacitor. Does the ac voltage gain A_V change if R_E is reduced by 10%? If yes, how many % up or down?

yes, $\approx 10\%$ up

- A common collector BJT amplifier features the following properties: (mark all that apply)

- A) high voltage gain
- B) high current gain
- C) low input resistance
- D) low output resistance

- A BJT features an Early voltage of 60V and an I_{CQ} of 1mA. How much does I_C change if V_{CE} increases by 3V while V_{BE} remains constant?

$\Delta I_C = +50 \mu A$

- Find the transconductance g_m of a BJT biased at $I_{CQ} = 5 \text{ mA}$ ($V_T = 30 \text{ mV}$).

$g_m = 0.167 \text{ S}$

- How much does the bias current of the BJT circuit in problem 2) change if V_{BE} increases by 50mV while V_{CC} and all resistors remain the same?

$\Delta I_C = -5 \mu A$

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1) a) CE config. $\left\| \begin{array}{l} r_i = \beta / g_m = \beta \frac{V_T}{I_{CQ}} = 5 \text{ k}\Omega \\ r_o = \frac{V_A}{I_{CQ}} = 100 \text{ k}\Omega \end{array} \right\| \begin{array}{l} 2 \\ 1 \end{array}$

b) CS config. $\left\| \begin{array}{l} r_i = \frac{\alpha}{g_m} = 49.5 \Omega \\ r_o = (1+\beta) \frac{V_A}{I_{CQ}} = 10.1 \text{ Meg}\Omega \end{array} \right\| \begin{array}{l} 2 \\ 2 \end{array}$

c) $\left\| \begin{array}{l} V_2 = -k \cdot r_i \cdot r_o \\ V_1 = r_i \cdot r_o \end{array} \right\| \therefore \left\| \frac{V_2}{V_1} = -k \frac{r_o}{r_i} \right\|$

common base config. $|k = -\alpha|$

$\left\| \frac{V_2}{V_1} = \alpha \frac{r_o}{r_i} = \alpha \frac{(1+\beta) V_A}{\alpha V_T} = (1+\beta) \frac{V_A}{V_T} = 202,000 \right\| \quad \text{J}$

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$$2) a) \quad \left| I_{CQ} = \frac{V_{CC} \frac{R_2}{R_1 + R_2} - V_{BEQ}}{\frac{R_1 \parallel R_2}{\beta} + R_E \left(1 + \frac{1}{\beta}\right)} = \frac{1.1V}{10.25k\Omega} = 107 \mu A \right| \quad 2$$

$$\left| V_{CEQ} = V_{CC} - I_{CQ} (R_C + \left[1 + \frac{1}{\beta}\right] R_E) = 3.55V \right| \quad 1$$

$$b) \quad \left| C_i = \frac{1}{2\pi f_c \cdot R_{in}} \right|$$

$$\left| R_{in} = R_B \parallel (r_i + \left[1 + \frac{1}{\beta}\right] R_E) = 14.5k\Omega \right|$$

$$\left| C_i = 109nF \right| \quad 3$$

$$c) \quad \left| r_o = \frac{V_A}{I_{CQ}} = 560.7k\Omega \gg R_C \right|$$

neglect r_o (assume $V_A = \infty$)

$$\therefore \left| A_v \approx - \frac{g_m \tilde{R}_L}{1 + g_m R_E \left(1 + \frac{1}{\beta}\right)} \right| \quad \text{where } \tilde{R}_L = R_C \parallel R_L \quad 2$$

$$\tilde{R}_L = 33.3k\Omega$$

$$g_m = 3.57mS$$

$$\left| A_v \approx -3.2 \right| \quad 2$$

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$$3) a) \left| \begin{array}{l} I_{CQ} \approx I_0 + \frac{V_E - V_{EE}}{1k} \\ V_E = -\frac{1k}{\beta} I_{CQ} - V_{BEQ} \end{array} \right| \quad V_{EE} = -5V$$

$$\therefore I_{CQ} = \left(I_0 - \frac{V_{BEQ}}{1k} - \frac{V_{BEQ}}{1k} \right) \frac{1}{1.01}$$

$$\| I_{CQ} \approx 105.3 \text{ mA} \| \quad \| V_{CEQ} = V_{CC} - V_E \approx 6.7V \| \quad 2$$

$$b) \left| \pi_{in} = \frac{\beta}{g_m} + (1+\beta) r_e \parallel R_L \right| \quad r_e = 1k\Omega$$

$$\| \pi_{in} \approx 4.8k\Omega \| \quad 2$$

$$\left| R_{out} = r_e \parallel \left(\frac{1}{g_m} + \frac{1k}{1+\beta} \right) \right|$$

$$\| R_{out} \approx 10.4\Omega \| \quad 2$$

$$c) \left| A_v = (1+\beta) \frac{r_e}{r_e + R_L} \right|$$

$$\| A_v \approx 96 \| \quad 3$$

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